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Ryan S. Loveless

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UNITED STATES NONPROVISIONAL PATENT APPLICATION

ON

A DEVICE FOR INTERROGATING THE LOCKED CONDITION OF A
VEHICLE SAFETY BELT BUCKLE

BY

Robert Hartmann
Martin Zapf

64646.00002 RSL

ATTORNEY DOCKET NO.:
64646.00002

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TECHNICAL FIELD OF THE INVENTION

This invention relates in general to safety belt buckles and more specifically to a device for interrogating the locked condition of a safety belt buckle for vehicles.

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BACKGROUND OF THE INVENTION

Two principles are known in the state of the art for recognizing the locked condition of safety belt buckles. On the one hand electro-magnetic switching contacts are used, which in their construction represent a mechanical belt buckle switch. In this, the locked condition is measured by means of an integrated micro-switch, a push button switch or a button. Such devices are known, for instance, from the German Patent Application DE 100 58 978 A1. On the other hand, in recent times Hall sensors with moving magnets are mainly used. Such devices are known for example from European Patent EP 0 842 832 B1, the European Patent Application P 0 861 763 A2, the PCT application WO 99/55561 and the German Patent Application DE 100 58 978 A1. In these, the locked condition is either directly or indirectly interrogated via the ejector. Because of the combination of magnets and moving provisions for the magnets, for example a compression spring, the construction is multi-part.

Fundamental problems occur in the above approaches. The traditional systems are sensitive to interfering external magnetic fields because of the operating principle. For example, if an electrical device is close to the belt buckle, it cannot be obviated that a interfering magnetic field overlays or diverts the magnetic field of the Hall sensor in such a manner that the Hall sensor no longer correctly recognizes the condition.

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In addition, indirect interrogation systems do not permit unambiguous interrogation of the condition of the locking component as they are used indirectly. If the activating component of the sensor fails to operate for 5 any reason, for example wear, fatigue or dirt, the sensor cannot recognize the true condition. If, for example, the activation of the ejector for the moveable magnet is interrupted, the Hall sensor recognizes a permanently open seat belt buckle. If the compression spring become 10 fatigued, the moveable magnet is moved from its position when the buckle is unfastened and the Hall sensor recognizes a permanently locked seat belt buckle. In the same way the operating principle does not provide a clear and precise switching point.

15 Furthermore, systems are known from the state of the art which have a sensor which registers the change in the direction of a magnetic field as a change in the electrical resistance of the sensor. The magnetic sensor uses an anisotropic magnetic effect and an auxiliary magnet. Such sensors are, for example, known from the 20 European Patent Application EP 1 125 802 A2. These systems require the presence of a bias / auxiliary magnet.

However, magnets are subject to numerous of 25 processes, for example such as ageing whereby the strength of the magnet declines. To ensure a recognition being reliable to a certain extent even in the presence

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of interfering magnetic fields, the contribution of a magnetic shield plate is suggested.

In addition, the anisotropic effect is rather small, in the region of a few percent ($\sim 5\%$), and dependant on 5 environmental parameters, for example temperature, thereby placing further demands on the evaluation circuit.

The results of faulty recognition of the locked condition could, for example, include the failure of an 10 airbag to be released in the case of an accident.

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SUMMARY OF THE INVENTION

From the foregoing it may be appreciated that a need has arisen for an interrogation system for recognizing the condition of the locking component of a seat belt buckle.

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According to one aspect of the invention, a device has been provided for recognizing the locked condition of a seat belt buckle. The device in this aspect includes a sensor that directly interrogates the condition of the 10 seat belt buckle by a change in inductance.

According to another aspect of the invention, a seat belt buckle has been provided. The seat belt buckle includes a seat belt buckle carrier, a seat belt buckle tongue, an ejector, a locking component, and a device for 15 recognizing the locked condition of a seat belt buckle. The device in this aspect includes a sensor that directly interrogates the condition of the seat belt buckle by a change in inductance.

According to another aspect of the invention, a 20 device has been provided for recognizing a condition of a safety belt buckle. The device in this aspect includes a sensor that directly interrogates a locked condition by a change in a coupling factor.

According to another aspect of the invention, a seat 25 belt buckle has been provided. The seat belt buckle includes a seat belt buckle carrier, a seat belt buckle tongue, an ejector, a locking component, and a device a device for recognizing the locked condition of a seat

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belt buckle. The device in this aspect includes a sensor that directly interrogates a locked condition by a change in a coupling factor.

The present invention provides a profusion of 5 technical advantages that includes an interrogation system for recognizing the condition of the locking component of a seat belt buckle which is insensitive to strong external magnetic fields.

Another technical advantage of the present invention 10 includes an interrogation system for recognizing the condition of the locking component of a seat belt buckle which interrogates the locking component directly.

Another technical advantage of the present invention includes an interrogation system for 15 recognizing the condition of the locking component of a seat belt buckle which which can be integrated into a seat belt buckle.

Other technical advantages are readily apparent to one skilled in the art from the following figures, 20 description, and claims.

BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present invention and the advantages thereof, reference is now made to the following brief description, taken in connection with the accompanying drawings and detailed description, wherein like reference numerals represent like parts, in which:

Figure 1 is a state of the art locked safety belt buckle;

Figure 2 is a state of the art unlocked safety belt buckle;

Figure 3 is an embodiment of a locked safety belt buckle according to an aspect of the invention whereby

Figure 3a is a side view,

Figure 3b is a plan view with the section B-B marked and

Figure 3c is a side view along the section B-B;

Figure 4 is an embodiment of an unlocked safety belt buckle according to an aspect of the invention whereby

Figure 4a is a side view,

Figure 4b is a plan view with the section A-A marked, and

Figure 4c is a side view along the section A-A;

Figure 5 is a sensor circuit using the oscillation principle; and

Figure 6 is an embodiment of a sensor circuit.

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DETAILED DESCRIPTION OF THE INVENTION

It should be understood at the outset that although an exemplary implementation of the present invention is illustrated below, the present invention may be 5 implemented using any number of techniques, whether currently known or in existence. The present invention should in no way be limited to the exemplary implementations, drawings, and techniques illustrated below, including the exemplary design and implementation 10 illustrated and described herein.

According to one aspect of the invention, a change in inductance is achieved by the interaction of one of the materials identified below with a sensor, based on this interaction a statement regarding the status of the 15 locking component can be made, as the change in inductance is directly interrogated by locking the seat belt buckle tongue in the seat belt buckle.

Diamagnetic, paramagnetic as well as ferromagnetic materials can in principle be used to change inductance. 20 Different levels of effect and different effects are produced by the selection of the material. If a diamagnetic material is used, the inductance reduces. If a paramagnetic material is used, the inductance increases. If ferromagnetic materials are used, the 25 inductance increases significantly.

Alternatively, the change of the magnetic coupling factor k of two coupled coils can be used in place of the change in inductance. The coupling factor k describes the

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relationship of the magnetic couplings between two electrical circuits 1 and 2. The following formula applies for the coupling factor between two electrical circuits with inductances L_1 und L_2 and the mutual

5 inductance M_{12} :

$$k = \frac{M_{12}}{\sqrt{L_1 L_2}}$$

In principle, diamagnetic, paramagnetic as well as ferromagnetic materials can be used to change the coupling factor k . Different levels of effect and 10 different effects are produced by the selection of the material. If a diamagnetic material is selected, the coupling factor k reduces. If a paramagnetic material is used, the coupling factor k increases. If ferromagnetic materials are used, coupling factor k reduces 15 significantly.

The effects described above are of a static nature and therefore enable the condition to be recognized precisely.

The operating principle of a state of the art safety 20 belt buckle can be seen in Figures 1 and 2. The following initially describes the locked condition in Figure 1.

The seat belt buckle consists of a seat belt buckle carrier (1) and a seat belt buckle tongue (2). The seat belt buckle carrier (1) comprises an integrated ejector 25 (3) and a locking component (7). A moveable magnet (5) is provided in between the ejector (3) and a compression spring (4). The magnet (5) is arranged in such a way that

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its position relative to a suitably positioned Hall sensor (6) can be altered by the ejector (3) and the compression spring (4).

In order to lock the seat belt buckle, the seat belt buckle tongue (2) is introduced into the seat belt buckle carrier (1) in accordance with Figure 1. This causes the position of the ejector (3) to change at the same time. The locking component (7) is locked. The ejector (3) in turn changes the position of the moveable magnet (5), which is now moved against the resistance of the compression spring (4). A suitably positioned Hall sensor (6) recognizes the position change of the moveable magnet (5) as a change in the field density and generates an electrical output signal, which indicates the locked condition.

If the locking component (7) is unlocked, the seat buckle tongue (2) can be withdrawn from the seat belt buckle carrier (1) as shown in Figure 2. A compression spring - not shown in the Figures - changes the position of the ejector (3). Further on, the compressed compression spring (4) changes the position of the moveable magnet (5). A suitably positioned Hall sensor (6) recognizes the change in the density of the field and generates an electrical output signal, which indicates the unlocked condition.

This output signal can be further processed in a suitable control device.

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A device corresponding to an aspect of the invention for recognizing the condition of a seat belt buckle is described below in Figures 3a - 3c and Figures 4a - 4c. The present invention solves the problems mentioned above 5 by the use of a sensor for the direct interrogation of the condition of a seat belt buckle. In particular, exact switching points can be realized and costs can be minimized with the device.

An embodiment according to an aspect of the 10 invention consists of a seat belt buckle carrier (1) and a seat belt buckle tongue (2). The seat belt buckle carrier (1) comprises an integrated ejector (3), a locking component (7), a leaf spring (8) and a sensor (9). The sensor (9) is for example a printed circuit 15 arranged in such a manner that the position of the seat belt buckle tongue (2) can be changed in relation to the sensor (9).

In addition, the locking component (7) or the leaf spring (8) or both can be made from a material, which 20 changes the inductance or the coupling factor.

The device is described below using a change of inductance.

In order to lock the seat belt buckle, the seat belt buckle tongue (2) is introduced into the seat belt buckle carrier (1) of a seat belt buckle according to an embodiment of the an aspect of invention in accordance 25 with Figures 3a-3c. The locking component (7) is locked and the leaf spring (8) is moved away from the sensor (9)

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as shown in Figure 3c. This change in position of the leaf spring (8) is recognized by the sensor (9) and a suitable evaluation circuit generates an electrical output signal, which indicates the locked condition.

5 If the locking component (7) is unlocked, the seat buckle tongue (2) can be withdrawn from the seat belt buckle carrier (1) in accordance with Figures 4a - 4c. The tensioned leaf spring (8) moves towards the sensor (9) as shown in Figure 4c. This change in position of the 10 leaf spring (8) is recognized by the sensor (9) and a suitable evaluation circuit generates an electrical output signal, which indicates the locking condition.

The electrical output signal can be further processed in a suitable control device.

15 A sensor layout in accordance with an aspect of the invention is explained below.

In a particularly preferred embodiment a planar inductive sensor $L(x)$ is positioned on a circuit board as shown in Figure (5). The inductance is applied as a 20 multi-turn conductor loop in a planar manner on a printed circuit. Such sensors are, for example, described in the German Patent Application 102 423 85 by the applicant. In this, the inductance L changes depending on the distance x of a suitable activating component for the inductance 25 L . In an aspect of present invention the leaf spring (8) is activated by the locking component (7). Depending on position x of the leaf spring (8) relative to the sensor (9), the inductance L of the sensor (9) varies.

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In this, the sensor (9) is positioned between the seat belt buckle carrier (1) and the leaf spring (8) and joined with the carrier. The seat belt buckle carrier (1) itself comprises a groove at the position of the sensor 5 as well as a recess at a small distance, for example 2 mm, relative to the face of the sensor (9) whereby inductive circular currents can be rejected.

The signal from the sensor (9) can now be processed in an evaluation circuit described below.

10 The change in the inductance $L(x)$ can, for example, be evaluated by a simple LC oscillator circuit. Such a circuit is presented schematically in Figure 5 (c) and comprises an inverted amplifier V , a resistance R , two ceramic capacitors C_1 and C_2 and the inductance $L(x)$. The 15 inductance is, for example, achieved by a printed circuit with an unattenuated inductance of $1 \mu\text{H}$ whereby the capacitors C_1 and C_2 and the inductance $L(x)$ form a π -network, and the output of the π -network is fed back to an inverted amplifier.

20 Such LC oscillator circuits must meet an amplitude- and a phase- condition (cf. Tietze/Schenk: Halbleiter-Schaltungstechnik; Springer Verlag, Berlin, 10th edition, Chapter 15.1 ff) so that on the one hand oscillation starts and on the other hand oscillation continues in a 25 stable manner.

1. The loop gain of the overall circuit must be greater than one.

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2. The voltage U_4 must be in phase with the voltage U_1 even in the case of an interrupted feedback arm.

The first condition referred to as the amplitude-condition and the second condition as the phase condition 5 of the oscillator circuit.

If the π - network is resonant, the voltages U_3 and U_4 are in opposite phase. The inverting amplifier V shifts the voltage again by 180° , and so in the case of low resistance R the voltages U_2 and U_3 are in phase. Thus the 10 phase condition is met.

The amplitude condition is met with low resistance R, an amplification V, which is greater than 2 and with a sufficiently large input resistance of the inverting amplifier.

15 The amplitude of voltage U_2 is increased by the factor " $-V$ " in comparison with the amplitudes of voltage U_1 by the inverting amplifier V. If the Q value of the π -network is high, the amplitudes of the voltages U_3 and U_4 are approximately equal. If the resistance R is small, 20 the voltage drop over the resistance R is small and so the amplitude of voltage U_2 is greater than the amplitude of voltage U_3 .

The oscillation conditions of the oscillator circuit may be violated if the resistance R is increased.

25 The resistance R and the capacitor C_1 form an RC-network. An additional phase shift therefore occurs between the voltages U_1 and U_3 when the resistance R is increased. If the phase shift reaches a certain value,

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the phase condition is violated and the oscillation ceases. This state is reached at the latest when the voltages U_1 and U_4 run into negative feed-back when the feed-back is interrupted.

5 In a similar manner, an increase in the resistance R produces an increased voltage drop in the resistance R . The amplitude of the voltage U_3 reduces. If the relationship of the voltage amplitudes U_2 to U_3 decreases under the influence of the amplification factor V , the
10 loop amplification drops under 1, thus violating the amplitude condition.

15 In an embodiment of the oscillator circuit the resistance R is set at such a level when the seat belt buckle (1) is closed that the oscillator oscillates in a stable manner. If the seat belt buckle (1) is opened, the leaf spring approaches the sensor and the inductance $L(x)$ is thereby reduced. The resonance frequency of the π -network increases. The oscillator oscillates at a higher frequency.

20 The change in the oscillator frequency can be used to evaluate the locking condition of a seat belt buckle. If, for example, a micro-controller (μC) is connected to the output of the π -network, the frequency of the voltage U_4 can be measured. Therefore, a thresh-hold value
25 is determined which lies between the "closed" and the "open" condition of the seat belt buckle. If the frequency varies over this thresh-hold, this is signaled

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by the micro-controller via a data bus or by another suitable analogue signal.

In a further, particularly preferred embodiment of the oscillator circuit, the condition of the seat belt buckle is evaluated by the condition of the oscillation.

The phase displacement of the RC- network is increased by an increase in the frequency also. Through this, at a suitable magnitude, the phase- condition of the oscillator circuit is no longer met and the oscillation ceases.

In addition, the cease of the oscillation due to the non-compliance of the amplitude- conditions can also be caused by suitable dimensioning of the components.

If invertors with frequency-dependant amplification are used, such as, for example, invertors of type 74HCU04, the amplification reduces significantly at frequencies greater than 12 MHz.

If the leaf spring (8) approaches the sensor (9), the frequency increases significantly, for example. As the frequency increases significantly, the amplification reduces significantly. At a suitable dimensioned resistance R, the loop amplification becomes less than 1 and the oscillation ceases.

A simple downstream differentiating circuit can be used to recognize if the oscillator is still oscillating. The oscillation condition, and therefore the condition of the seat belt buckle (1) can be indicated, for example,

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by an LED or an audible warning, or be transmitted to a control facility by a digital signal.

The above circuits represent a one- port- network with regard to the inductance changes.

5 In a further, alternative embodiment of the sensor (9), the change in the magnetic coupling factor can be also achieved as represented schematically in Figure (6) and as described in German Patent Application DE 101 25 278 filed by the applicant, by the change in the magnetic 10 coupling factor of two coupled coils applied in a planar manner instead of by the change in the inductance, caused by the approach of the leaf spring (8). This circuit represents a two- port- network with regard to the inductance changes.

15 A corresponding sensor circuit comprises the following components which are depicted in Figure (6): a high frequency current generator $Q\sim$, a feed coil E, a sensor coil S, an amplifier V, an amplitude detector D and a controller A.

20 The current generator $Q\sim$ generates a high-frequency alternating current which is passed through the feed coil E. This alternating current generates a magnetic field H1, which induces an inductance voltage in the sensor coil. The amplitude of the voltage is dependant on the 25 coupling factor, amongst other things. This inductance voltage is amplified by an amplifier V and passed to the amplitude detector D. The amplitude detector D generates a DC voltage signal, which corresponds with the amplitude

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of the inductance voltage except for an off-set. This DC voltage signal is further evaluated by the controller A. If the DC voltage signal drops below a certain value, the seat belt buckle is open.

5 The high frequency current generator Q~ may, for example, supply a current of approximately 2 mA at a frequency of 12 MHz. For example 100 mV_{pp} are then induced in the sensor coil S. The controller A may, for example, be realized by a switching controller which indicates the 10 decrease in the DC voltage signal below a specific threshold via a bus or by an analogue signal. The sensor may be arranged by two multi-turn conductor loops E and S whereby the conductor loops are concentric, bifilar and planar, and are applied on a printed circuit.

15 If the seat belt buckle (1) is opened, the leaf spring (8) is close to the circuit board with the sensor (9) and attenuates the inductive coupling of the feed coil and the sensor coil. This causes the inductance voltage to drop, which in turn leads to a reduced DC 20 voltage at the output of the amplitude detector D and to a change over of the controller A.

 The embodiments of the sensor and suitable plotting circuits described above serve as an illustration. Further embodiments to use the principle of inductance, 25 variations in the materials and suitable evaluation circuits will immediately be apparent to a person skilled in the art.

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List of reference symbols

1	Seat belt buckle
2	Seat belt buckle tongue
5	Ejector
3	Compression spring
4	Moveable magnet
6	Hall sensor
7	Locking component
10	Leaf spring
8	Sensor
V	Amplifier
R	Resistance
C	Capacitor (C ₁ , C ₂)
15	L(x) Inductance
Q~	High frequency current generator
E	Feed coil
S	Sensor coil
D	Amplitude detector
20	A Controller

Although the preferred embodiment has been described, it should be understood that various changes, substitutions, and alterations can be made herein without departing from the scope of the present invention, even if all, one, or some of the advantages identified above are not present. These are only a few of the examples of

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arrangements and configurations that are contemplated and covered by the present invention.

The various components, configurations, and materials described and illustrated in the preferred 5 embodiment as discrete or separate parts may be combined or integrated with other components and configurations without departing from the scope of the present invention. Other examples of changes, substitutions, and alterations are readily ascertainable by one skilled in 10 the art and could be made without departing from the spirit and scope of the present invention.